

SECTION III

TOPOGRAPHY

Section Editor: Robert R. Stowe

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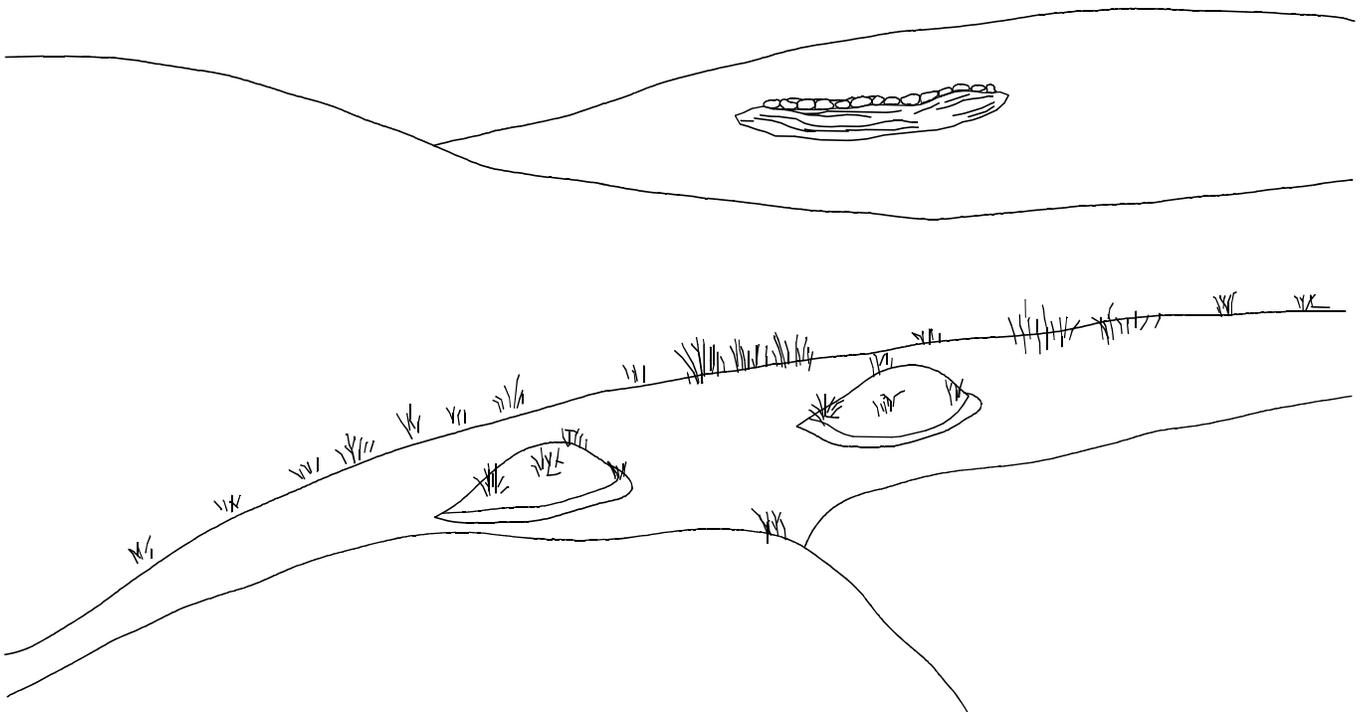


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A. Introduction

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Reclamation of western lands can be enhanced with some forethought as to what the topography will look like and how it will function with the proposed postmining land use. When land is being reclaimed from surface mining back into grazing land and/or wildlife usage, adding some macro- and micro-relief structures can be of benefit to both livestock and wildlife. Semi-arid conditions frequently mean few or no trees and strong winds. When there is little or no topographic relief to protect livestock and wildlife from the summer sun and the winter winds, animals suffer and may perish. Topographic relief can provide the protection required in addition to augmenting the postmining land use.

In areas where reclaimed lands will become farm land, topographic design is also important. In these situations, minor hills and slopes, as well as drainages, should be designed so that runoff from precipitation and snow melt will not inundate land to be farmed, and the reconstructed drainage-ways will not be overly erosive.

The following subsections discuss methods of shaping hillslopes in order to provide topographic diversity for wildlife and livestock while minimizing erosional features. A discussion of procedures used to compare the premining and postmining slope regime is also included.

NOTES

B. Hills/Slopes

1. Hillslope Shaping and Morphology

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#### **Situation:**

Landform stability is a critical element in the reclamation of mined lands. The hillslope is the uppermost unit of the basin watershed and is typically responsible for the production of sediment to the watershed. Concentrated flow or flowing water transfers this sediment to the first and second order stream channels and ultimately delivers the sediment to receiving waters outside the mine permit area. Where surface runoff remains in an unconcentrated condition, little sediment movement and virtually no transfer of sediment off-site will occur.

The intent of mining regulations is to minimize sediment production off mined and reclaimed lands, and to reestablish a hydrologic system which will behave in an erosionally stable manner equal to or better than that which existed prior to mining.

For the purposes of this handbook, the hillslope component of reclaimed basins is the upper watershed and valley sideslopes which deliver runoff to the smallest (first order) designed drainages in the reclamation plan. Where slope gradients or slope length exceeds some threshold value, surface water runoff will concentrate, producing rill and gully erosion. Hillslope shaping, and an understanding of slope morphology and processes, will reduce surface erosion on the hillslope.

#### **Special Considerations:**

Decisions regarding landform shaping reflect a balance of mine path, mining methods, geomorphic considerations, and economics. The operator must consider the locations and elevations of haulage roads, ramps, spoil piles, pre-existing and postmining basin outfalls and drainage divides. For example, mine production features such as haulage ramps and roads can often become components of the postmining drainage system. In these areas, backfill costs can be curtailed if postmining drainages are restored to incorporate a portion of the ramp or road alignment.

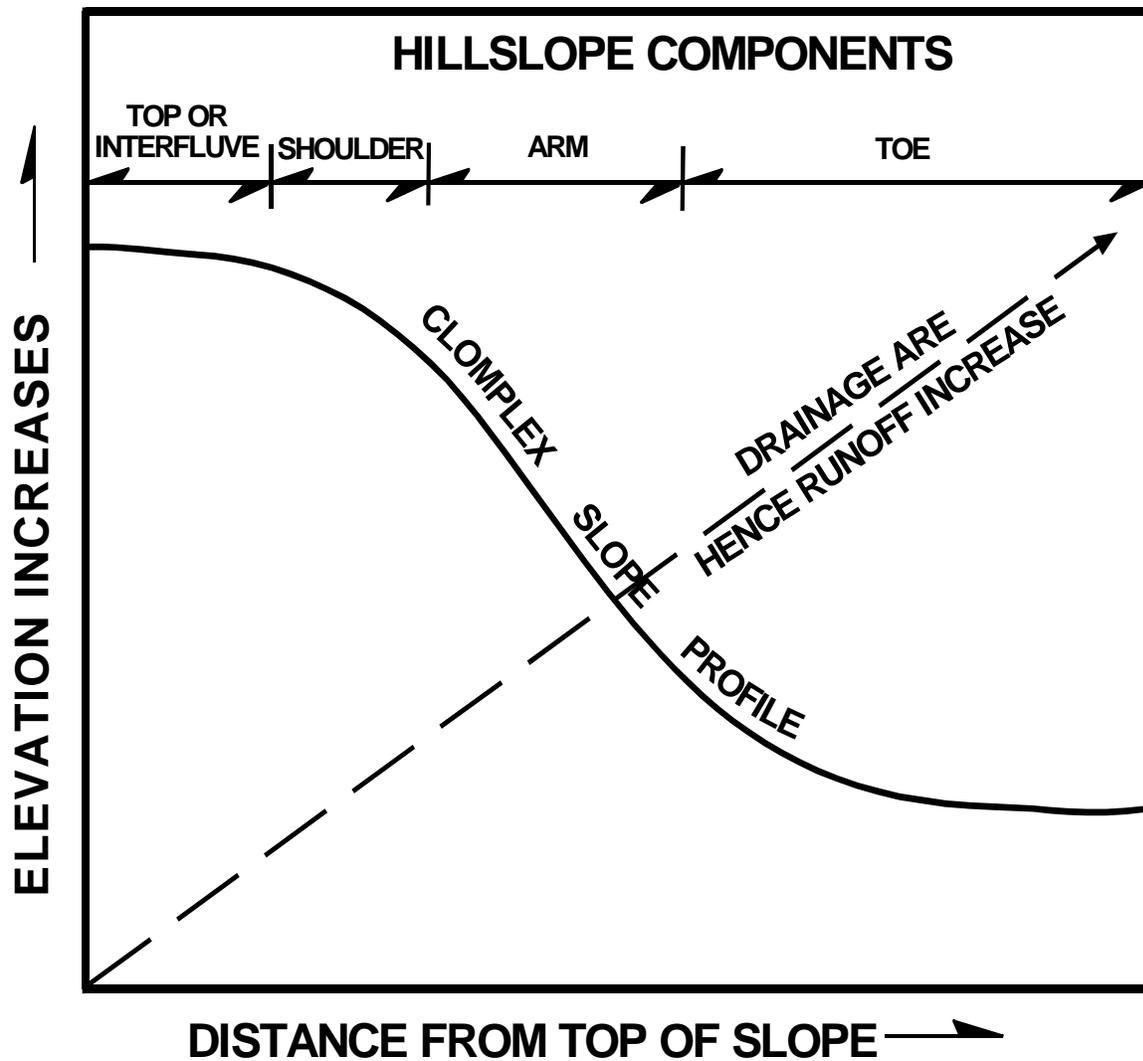


Figure 1. Hillslope Components  
(From Perrens, et. al., 1984)

Similarly, out-of-pit overburden stockpiles and/or dragline spoil dumps can be formed into the upper elevation or hillslope component of the drainage system. In doing this, the operator can minimize "double handling" and reduce hauling costs. Pit backfill sequencing should incorporate the final reclamation topography and address not only final drainage design but also final hillslope design.

The overall reclamation plan and hillslope design must reflect such critical variables as postmining basin outfalls and the topography of adjacent lands. Reclamation planning should consider basin or hillslope aspect. Final topography can be adjusted to accommodate the harsher conditions associated with increased solar and wind exposure. Experience suggests that there is a significant im

provement in reclamation success on protected slopes. Increased moisture retention is required on southern exposure slopes. This can be accomplished by flatter slope angles and a more roughened final reclamation surface.

### **Description of Technique:**

#### **a. Hillslope**

The hillslope is defined by a minimum of four subunits and the standard nomenclature (after Perrens, et.al. 1984) is presented on Figure 1. These particular units were first developed by agronomists in recognition of the importance of a soil's position on a natural hillslope with respect to soil genesis. Those soils, which develop near the shoulder and arm of the slope, are transported by both water and gravitational processes to the toe of the slope. In nature, soil horizons are thickest at the toe of the slope and thinnest at the shoulder.

When replacing topsoil on a reclaimed hillslope, it is typically replaced to a uniform depth. As natural erosion and depositional processes occur on the reclaimed hillslope, translocation of topsoil will take place and over time, the thicker zones will occur at the toe of the slope. Recognizing that these processes will occur, yet designing the slope to minimize the movement of topsoil by such accelerated processes as rill and gully erosion, is a critical design consideration.

The design philosophy should recognize the value of rainfall infiltration and the liability of direct surface runoff. Water retention on the hillslope will promote revegetation success, and by so doing will stabilize the reclaimed land surface. Where runoff occurs in a concentrated manner, excessive shear forces may occur, resulting in rill and gully erosion. Minimizing slope length and excessive slope gradients will prevent the concentration of direct surface runoff on the hillslope.

Design and construction considerations, which should be addressed in hillslope reclamation, are addressed in the following paragraphs.

(1) Hilltop or Interfluve

As a rule of thumb, the designer should maximize the acreage of the hilltop and minimize the overall slope length. The hilltop should be formed to retain the maximum moisture onsite with minimum delivery of runoff from the hillslope. In the field, this translates as grade staking the top of an overburden stockpile or dragline dump to ensure the flattest possible configuration (20H:1V or flatter) while maintaining an overall positive drainage. Leaving the regraded surface in a roughened condition will enhance its water retention capabilities. Immediately prior to the replacement of the topsoil, the overburden should be "deep-ripped" or scarified. The topsoil can be replaced directly on the rough overburden backfill surface (at variable thicknesses) and/or the replaced topsoil can be manipulated by mechanical farming methods. Reclamation success has been achieved with "pitting", which is a mechanical means of constructing actual soil pits or divots within the topsoiled surface. Pitting is accomplished simultaneously with drill seeding during final reclamation. Similarly, the construction of small intermittent dozer basins has successfully achieved the water retention goals and aided in the development of small playa-like features.

Where a greater acreage of interior drainage is required or desired, the replacement of well-drained soils is essential to prevent the unwanted accumulation of salts. Although natural playas and interior drainage features exhibit a predominance of clay soils, the elimination of salt accumulation will enhance revegetation efforts during the critical initial years of bond release. More information regarding topsoil replacement can be found in the Topsoil section of this handbook.

A final consideration in the geometry of the hilltop is an assessment of contributing basin area for the receiving drainages. Basin divides can be manipulated to increase the watershed area and peak flow hydrology of one basin while decreasing the watershed area and peak flow hydrology of the adjacent basin. If channel slopes are excessive in one basin, the designer might consider diverting part of the basin runoff to another basin, thereby decreasing the overall peak flow hydrology of that basin.

(2) Hillslope: Shoulder and Arm of Slope

To the extent possible, the designer should minimize the length of slope or reduce the slope steepness. Initial slopes on mine dumps typically range from angles of repose to 1.5H:1V. Minimum reclamation slopes are often controlled by equipment accessibility and the ability to "farm along the contour". Although minimum "farmable slopes" may range from 2.5H:1V to 3H:1V and are dependent on the farming equipment, vegetative success is more pronounced on 4H:1V or shallower slopes. Within arid and semi-arid reclamation, slope aspect plays an important part in vegetation success and 5H:1V or flatter minimums are found to be more successful on south aspect slopes. North-facing slopes can be slightly steepened and 4H:1V minimums have proven to be successful. Wherever possible, flatter slope gradients are highly recommended and will increase rainfall infiltration and decrease concentrated flow.

Slope length and slope shape are also critical design considerations. The slope shape and slope transitions should be designed to promote unconcentrated flow and to minimize the offslope delivery of sediment. Where the combination of critical slope characteristics (slope length, slope steepness and contributing area) will result in concentrated flow, the runoff and sediment should be collected into a first order channel and delivered in a controlled manner offslope. Small drainage reconstruction is discussed in the Hydrology section of this handbook.

Practical experience has shown that slope lengths in excess of 50 to 100 feet at gradients of 4H:1V or steeper may result in rill and gully erosion. At 5H:1V slopes, lengths in excess of 150 feet or more may be problematical. Of course, vegetation density, soil type, and storm intensity and distribution are important variables in this analysis. Coarse textured soils and/or successfully vegetated slopes will allow more latitude in slope length.

Cross-slope ditches or furrows can be incorporated into the hillslope reclamation to achieve the required slope lengths. Such ditches should be small and unobtrusive and should be constructed oblique to the contour.

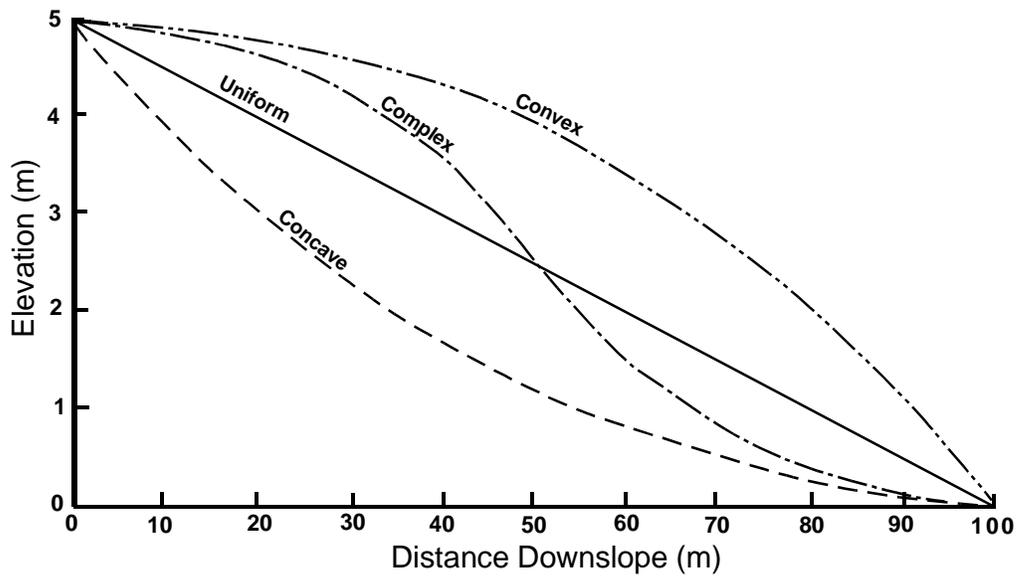


Figure 2a. Typical Hillslope Shapes.  
(From Perrens, et. al., 1984)

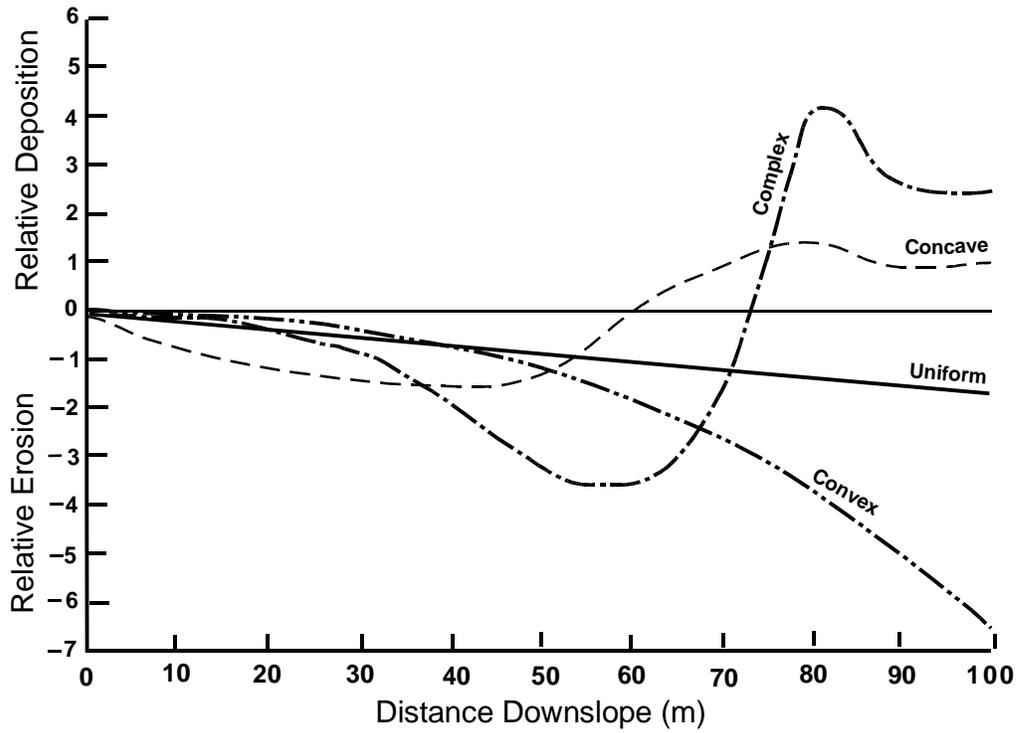


Figure 2b. Erosion / Deposition Mass Balance.  
(From Perrens, et. al., 1984)

In order to reduce the probability of ditch failure, a minimum gradient of four percent should be established for all cross-slope ditches. Flatter ditch slopes and contour ditches are difficult to construct, and tend to collect water in low spots created by settlement of the fill or poor staking/construction practices.

Figures 2a and 2b present typical hillslope shapes and a mass balance of erosion and deposition along the hillslope. The movement of sediment within the hillslope component is a function of both water and gravitational processes. From a practical standpoint, uniform and concave slopes are most often employed in mined land reclamation. Of these two slopes, the concave slope provides a more stable land surface as seen in Figure 2b. Complex slopes, which are more readily found in nature, exhibit increased erosion along the center or medial portion of the slope and increased deposition at the toe of the slope. If designed properly, a complex slope can be a stable entity within the overall reclamation scheme and provide diversity in the overall reclamation topography.

Uniform slopes are the easiest to stake and construct in the field. The slope configuration provides few depositional sites within the hillslope. However, where excessive slope lengths occur, offslope transport of sediment (erosion) can be anticipated (Figure 2b). Where uniform slopes are staked in the field, flatter gradients and adequate transitions at the toe must be incorporated. Figure 3a presents a 4H:1V uniform slope. Depending on slope length, basin aspect, and transition requirements, a flatter slope such as a 5H:1V or 6H:1V may be recommended.

Concave slopes may require additional staking and construction supervision, but provide better control of sediment movement and a more stable land surface (Figure 2b). The lower gradient portion of the slope allows water velocities to decrease, thereby enhancing depositional processes. The increased staking and construction supervision responsibilities may offset long term maintenance responsibilities. A variation of the concave slope might entail a 4H:1V slope from the interfluvial to the arm of the slope and a 5H:1V slope from the arm through the toe section of the slope. Practically speaking, in a multiple-benched mine dump, the upper lifts would be graded to a 4H:1V slope. The cut material would be relocated to the base of the dump and the 5H:1V toe slope would be created (Figure 3b). The point of inflection between the 4H:1V and 5H:1V slope (intermediate catch point) would be established based on an earthwork balance.

Complex slopes require intermediate cut stakes as well as the staking of each catch point (Figure 3c). Typically the construction of a complex slope may require additional earthwork, although there will be certain earthwork savings in the steep upper "shoulder" reach. The upper reaches of a complex slope provide maximum surface area for rainfall infiltration and minimum runoff. The arm of the slope is the steepest portion of the slope, yet will have limited drainage area contributing to direct surface runoff. Where runoff does occur, the hillslope gradients are the most gentle and velocities will be reduced.

(3) Hillslope: Toe of Slope

The construction of the toe of the slope is often the most essential aspect in hillslope reclamation. Too often the toe of the slope will be left in a convex or over-steepened form. This condition will often result in erosion, since the hillslope drainage basin area is the greatest at the toe of the slope. Because runoff increases with increased drainage area (Figure 1), it is essential that the slope gradient decreases at the toe of the slope. As noted in the previous sections, it is the design intent to maintain unconcentrated flow and promote infiltration. The lower gradients will also promote the deposition of hillslope sediment, thereby reducing sediment contribution to receiving drainages.

A second element in the construction of the toe of the slope is the smooth transition of the hillslope into the adjacent reclamation valley. A low gradient toe, which transitions into a stream valley, will allow lateral movement of a reclamation channel against the hillslope. If the slope enters the stream valley in an over-steepened condition, erosion and undercutting of the toe is likely to occur.

b. Summary of Hillslope Morphology

Hillslope design should maximize the opportunity for rainfall infiltration and minimize the opportunity for surface water runoff and flow concentration. The movement of sediment within the hillslope form is an essential geomorphic element in natural slope processes. Minimizing offslope movement via rill and gully erosion is critical, and will result in a reduction in sediment contribution to the receiving drainages.

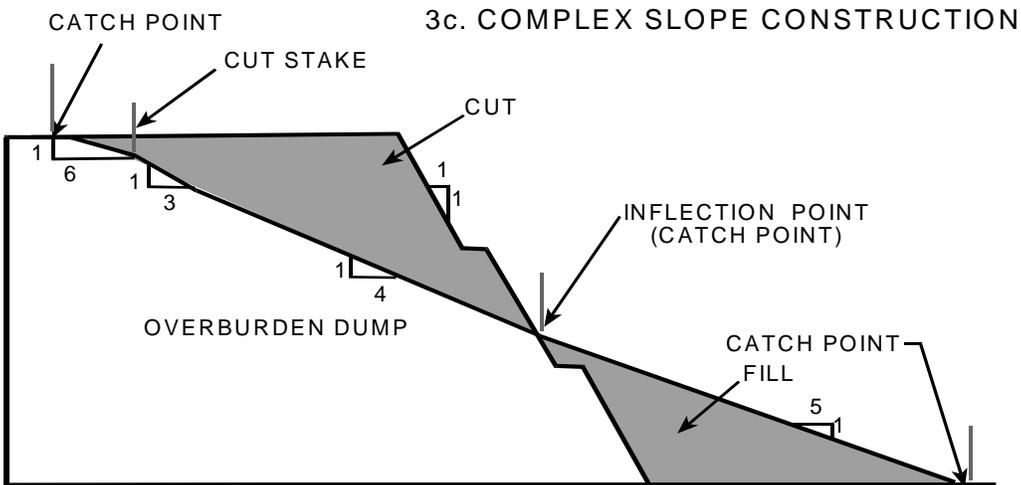
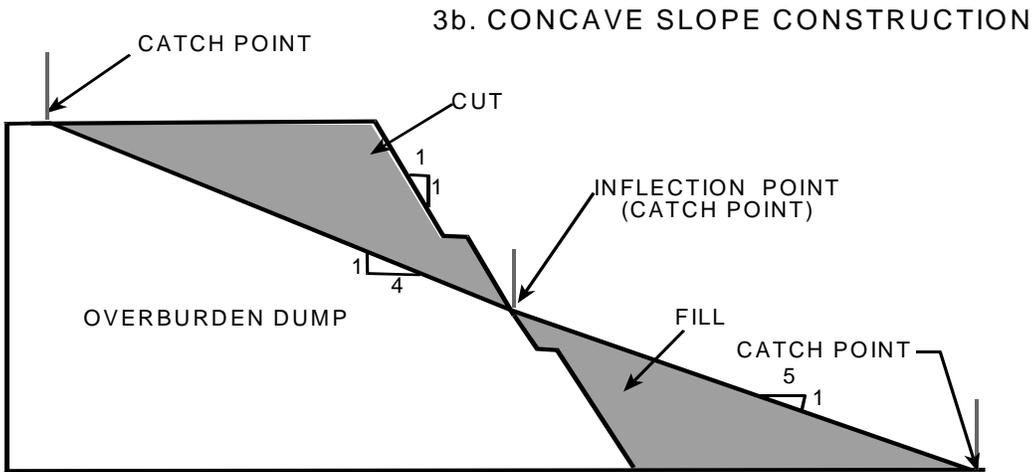
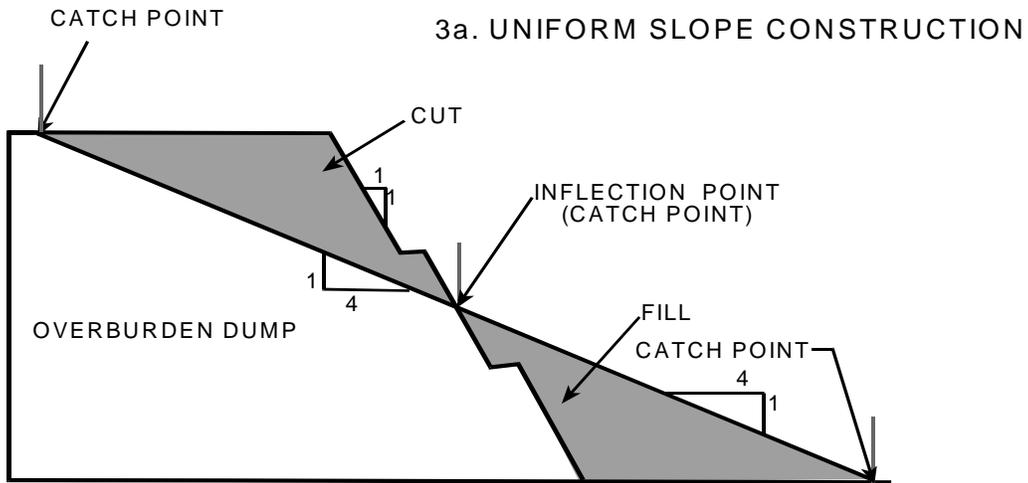


Figure 3. Reclamation Slope Construction

Figure 3 presents the three slope shapes discussed above and the minimum construction staking requirements. Although all three slope shapes are presented, the concave slope design best balances the economics of material movement with the design philosophy discussed above.

c. Construction Practices

Construction requirements are relatively simple and much work can be completed with a dozer. If dozers are used in construction, catch points should be staked in the field and adequate compaction is required near the toe. If scrapers are used in construction, additional staking to define cuts may be helpful.

Some compaction of the fill portion of the hillslope is essential to prevent or eliminate settlement, and in some cases failure of the fill. Concern with compaction is not as pronounced when construction by scrapers is employed. When backsloping a fill against a highwall, keying the fill into the rock highwall must be addressed. In certain instances where ground water is encountered, drainage below the fill must also be incorporated into the design.

## 2. Backfill Grading Observations

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Situation:

Relief techniques are an important tool in controlling erosion and cost. Planning a water course for drainage will facilitate preparation for the flow and reduction of erosional problems on reclaimed lands.

Costs can be controlled by planning for the placement of backfill and having the backfill dumped to grade as much as possible. The incremental haulage or handling cost of \$ 0.05 per yard is very economical compared to the \$ 0.25 to \$ 0.50 per yard cost of rehandling backfill.

Special Considerations:

Backfill will differentially settle, up to ten feet on a rare occasion; three feet is not unusual. Constructed topography features must be massive enough to function even with settling in critical areas. Plan ahead to know your desired topography. This will allow for maximum use of mine equipment for placing and grading backfill while that equipment is in the area. Finish grading of frozen backfill will likely take two to three times the equipment hours as compared to thawed backfill.

Description of Technique:

a. Dump Slope Grading

Dump grading can be made more economical by the selective placement of loose dumps and through dump grade control (see Figure 1). Dump grading volume can be reduced and maintained by using the following methods:

- (1) Decreasing the dump height by five to seven feet (loose dump height).

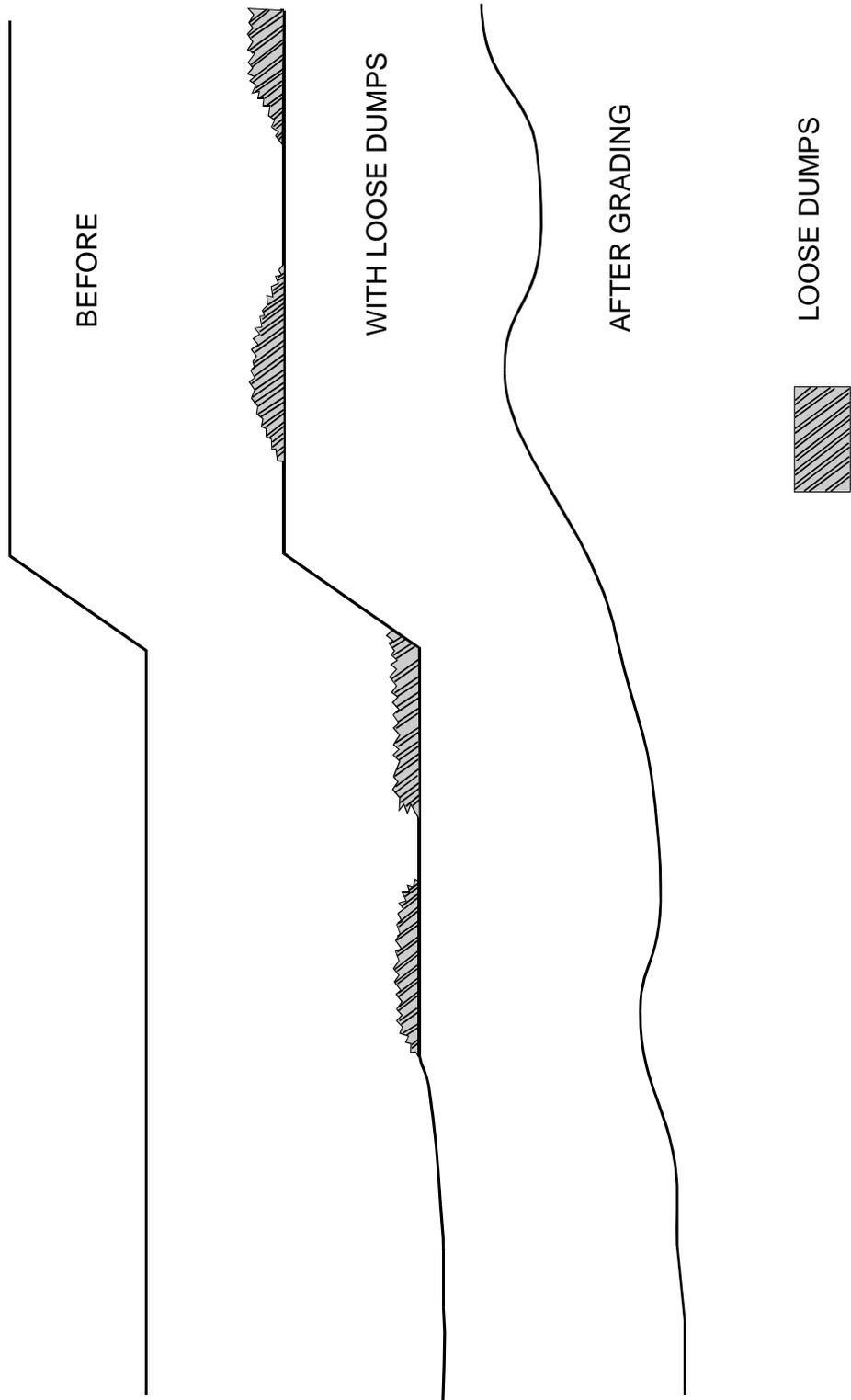


FIGURE 1
NO SCALE

- (2) Sloping the dump grade to be lower at edges and high where needed.
- (3) Placing loose dumps at the toe area, dump top, and ridge spots to reduce dozing needs and create micro-features and drainage control.

b. Second Bench

A second bench reduces reclamation grading volume by 70 percent (see Figure 2). In this case, the volume was reduced from 48 yards³ to 14 yards³ per linear foot of dump face with a 50 percent reduction in push length.

The second bench can be built between or after the main dump. However, if it is built first, it will reduce the overall cycle time of the haul trucks because they will not have to climb to the top to dump all loads of dirt. After the lower dump is in place, the toe limits of the second (top) dump are established on the second bench. Note that additional activity is required by a dump dozer during backfilling.

c. Dump Top Reclamation

For more information, see part a(3) in the subsection entitled "Small Drainage Waterway Construction" in the Hydrology section of this handbook.

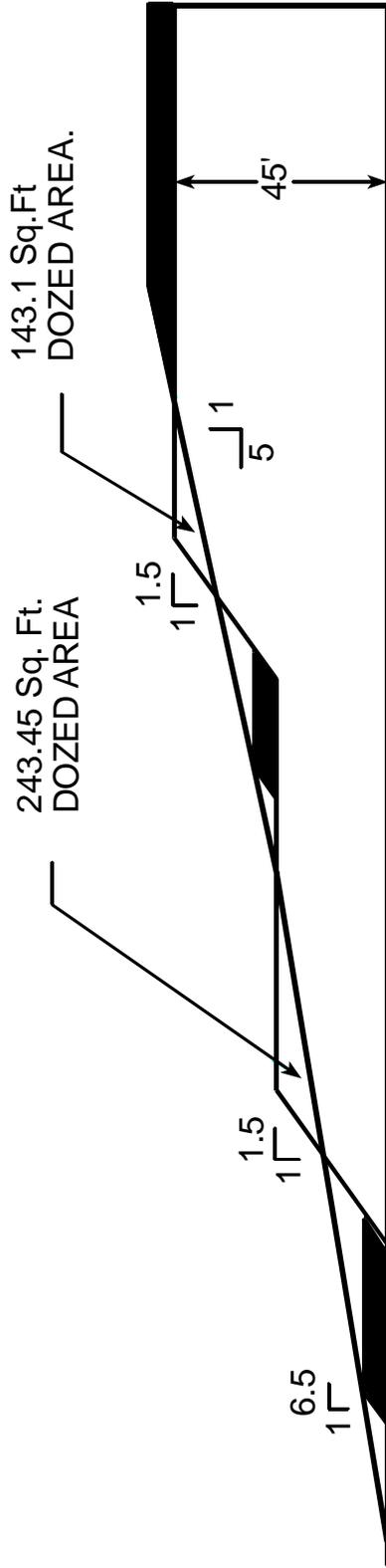
It is extremely important to limit the flat areas above slopes because concentrations of runoff down the slope will cause slope erosion. Generally there are two options, depending upon the width of the dump:

- (1) Grade to a hill (see Figure 3)
- (2) Grade to a hill with interior drainage (see Figure 3)

d. Long Slope Grading

For information on Long Slope Grading, please see part a(1) in the subsection entitled "Small Drainage Waterway Construction" in the Hydrology section of this handbook.

TOTAL OF 386.55 Sq. Ft. DOZED



LOOSE DUMPS 5' HIGH WITH A 5:1 SLOPE

SCALE= 1"=20"

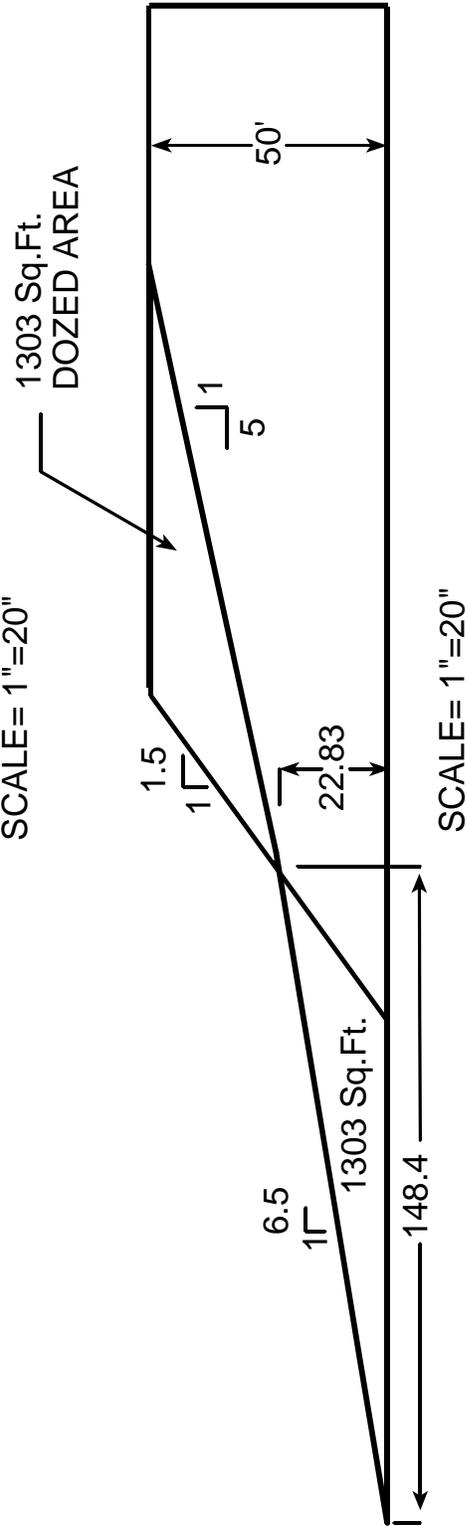


FIGURE 2

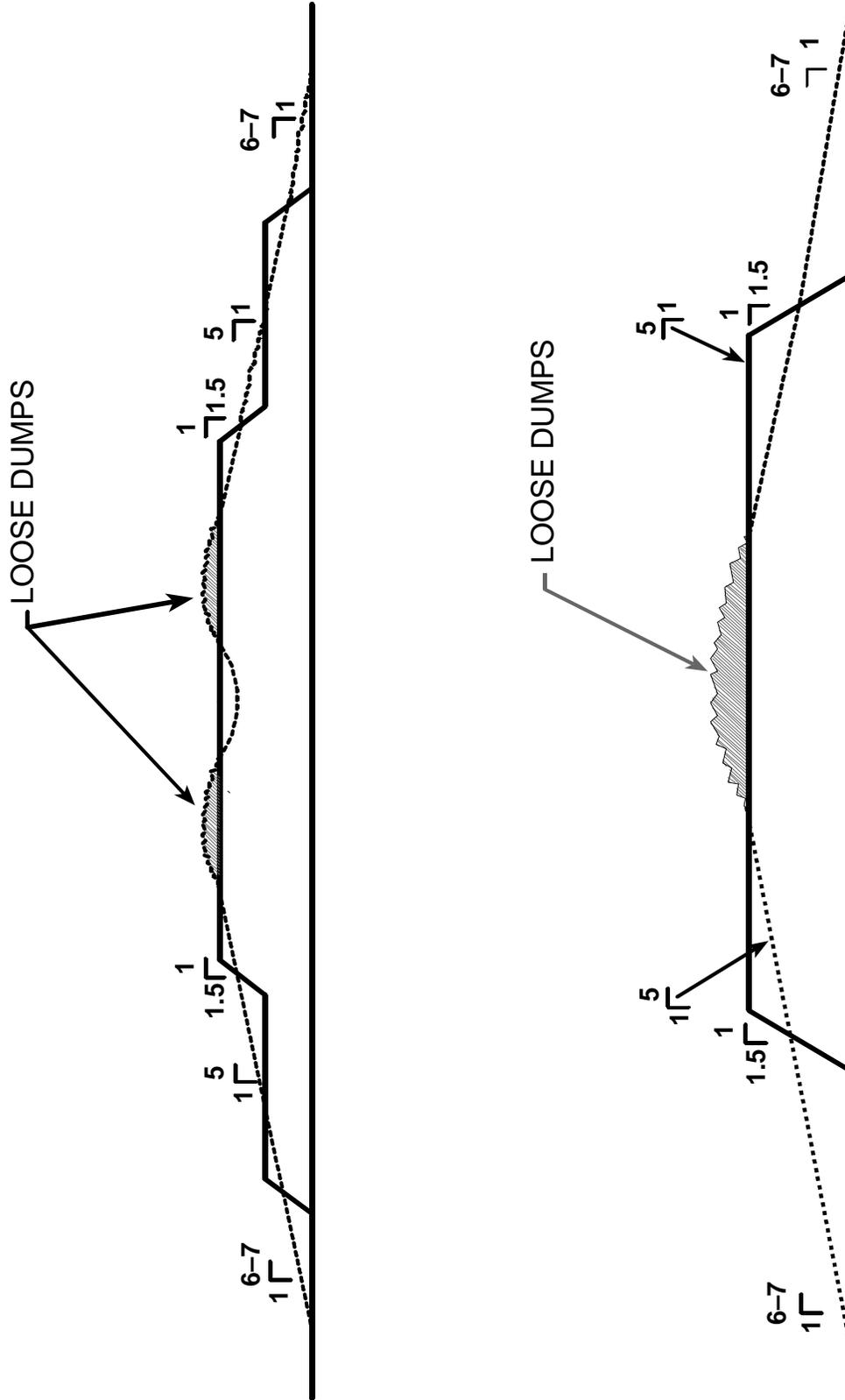


FIGURE 3
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NOTES

3. Evaluation and Comparison of Topographic Descriptive Methods

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#### **Situation:**

Mining reclamation requires a comparison between the premining and postmining slopes. This comparison is done to ensure the support of postmining land use. Reconstructed land must blend with native land and postmining slopes must be neither much steeper nor much flatter than original slopes.

#### **Special Considerations:**

These slope comparisons generally divide the land surface into a number of grid cells in order to calculate the slope, or rise divided by run, at the grid cell node. This information can then be mapped in several ways. Three methods for evaluating and comparing topography techniques are outlined below.

#### **Description of Technique:**

##### a. Evaluation and Comparison of Topography Techniques

From any of the following three techniques, tables and histograms can be generated to evaluate the percentage of topographic surface with certain slopes or features. Tables and histograms are especially useful when comparing two surfaces, for example premining and postmining topography. Many engineering firms are available to conduct these evaluations. Special engineering software packages are also available to do this work.

##### (1) Elevations

Slope value (and optionally, direction which yields a vector) must first be plotted for each grid node. The nodes for the grid and search radius should be selected so that averaging or smoothing between nodes conceals variability in the underlying topography. In one particular form of this method, slopes are calculated by first

estimating elevation values into a 100-foot grid from irregular contour data. These grid values are then subtracted from the nearest neighbor to provide a change in elevation in each cardinal direction. Elevation differences in north and south directions are added, then divided by the total difference between grid values (i.e. 200 feet), to provide a slope in the north-south direction. The same is done for the east-west direction. These component slopes are then added, via vector analysis, to yield the slope magnitude in percent and direction in degrees at the node being analyzed. Vectors may be drawn from each node pointing downslope, with the length of the vector denoting the steepness of the slope.

The above analysis is performed every 300 feet to separate posted data values sufficiently for plotting purposes (postmining values at a 100-foot spacing would require a very large map with no gain in accuracy or precision). Slope isopleths may be drawn by contouring the slope magnitude from the slope data on 300-foot centers. Slopes are calculated within projected disturbance limits only, and both pre- and post-mining slopes are calculated on identical 300-foot centers to allow direct comparisons. These values are then posted on a screened topo base map (see Figure 1). This dynamic map can provide insights as to what areas may become erosive and where deposition is likely to occur in a drainage.

(2) Isopleth Map

A second method is to contour the points of equal slope in an isopleth map. The contours on this map show the areas of increasing or decreasing slope. A plain with little relief would show few isoslope contours, whereas a quickly steepening bluff would be depicted by many isoslope contours. Water will flow perpendicular to the isoslope contour lines. This is illustrated in Figure 2.

(3) Mapping Geomorphic Features

A third method of evaluating topography techniques is to map geomorphic features, such as hills, slopes, ridges, saddles, valleys, and scarps on a topo base. This map will show areas where the various geomorphic features are located. Materials used to identify geomorphic features include a premining topographic map of scale 1"=1000' and numerous composite air photographs. Abandoned meanders shown on the premining landforms map are identified using USGS topographic maps of 1"=2000'. Meanders shown are those that were apparent on more than one map source and appear to be within the limits

of the most recent terrace deposits. This is more of a qualitative map than either of the two previous maps, as seen in Figure 3.

FIGURE 1

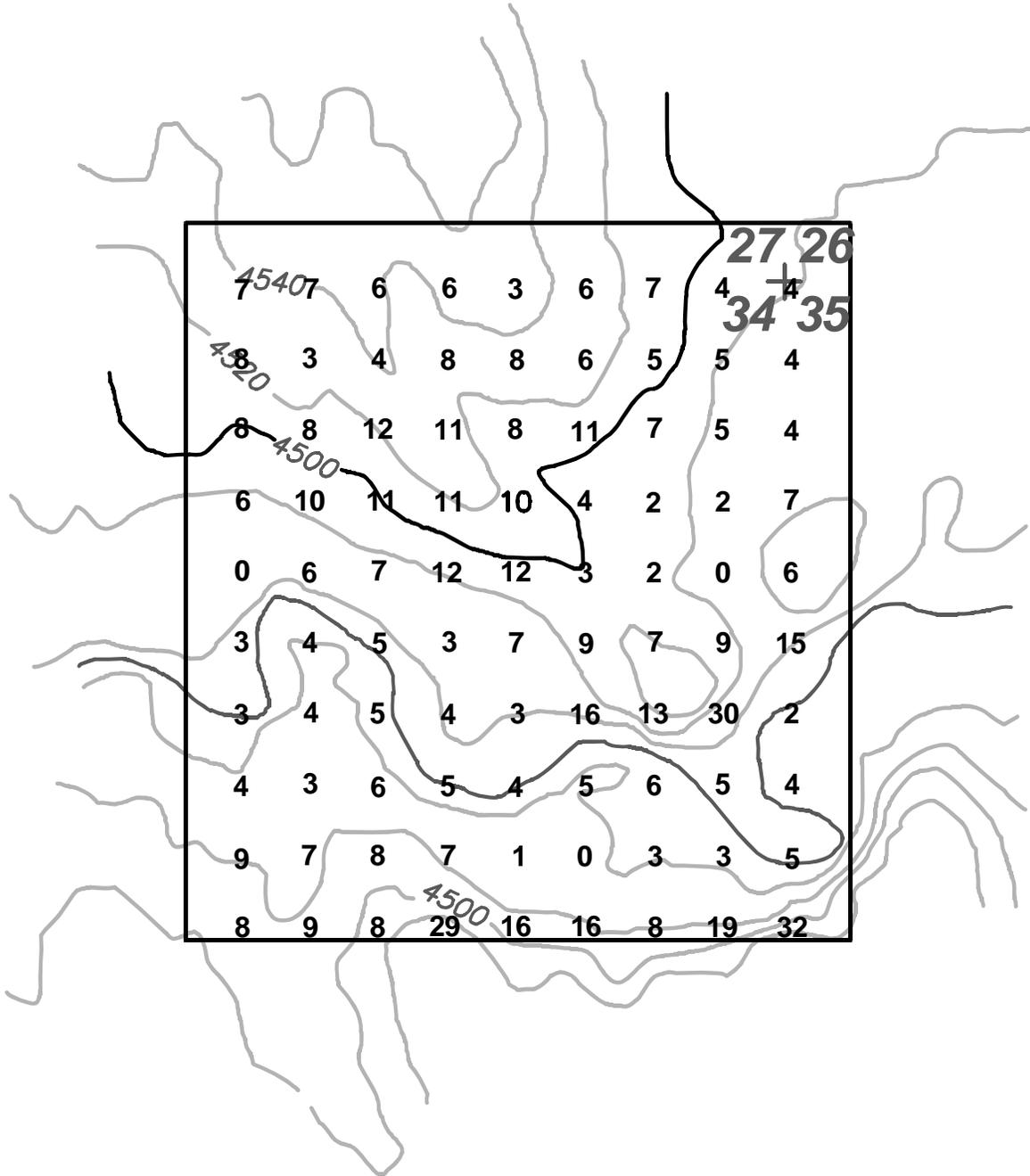


FIGURE 2

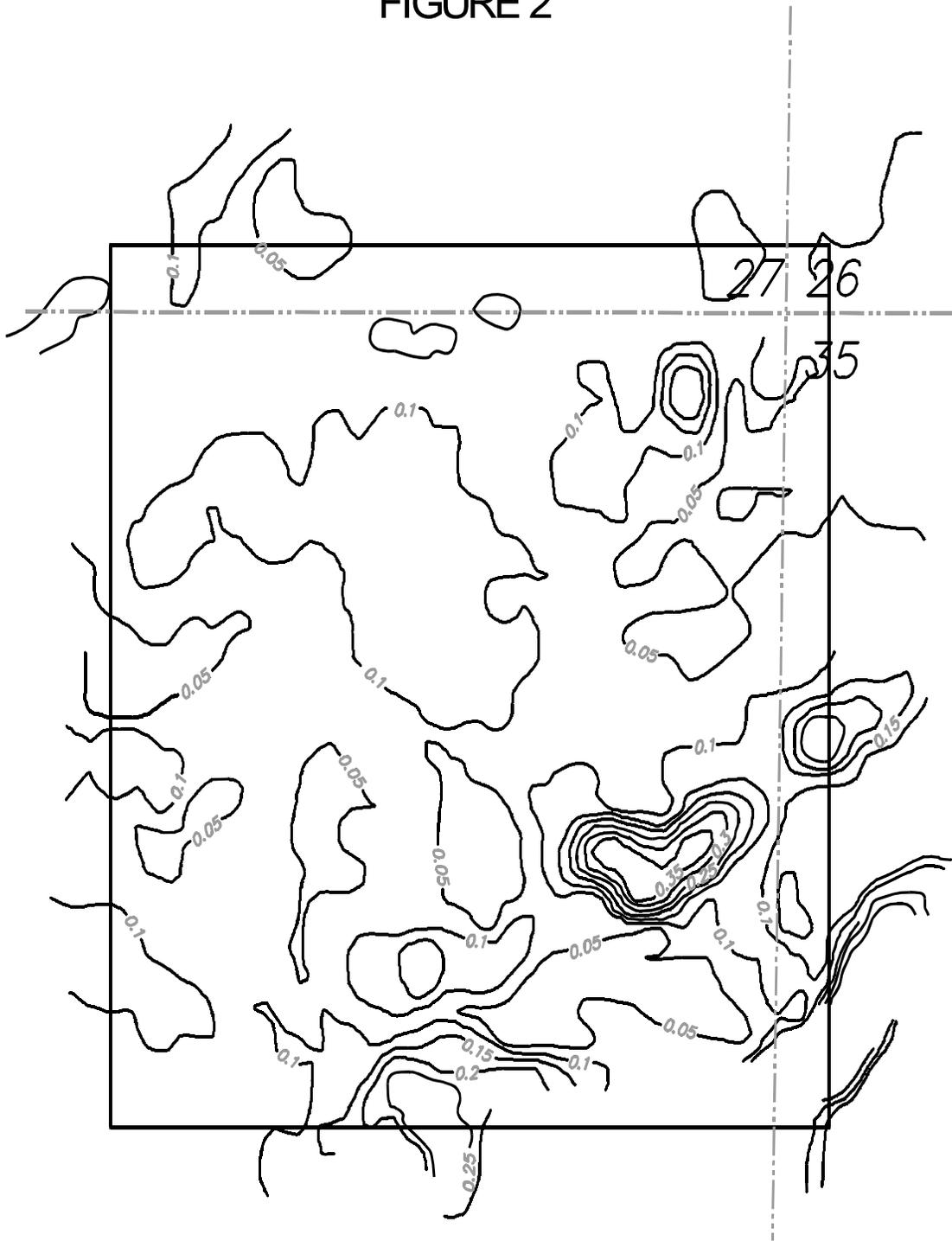
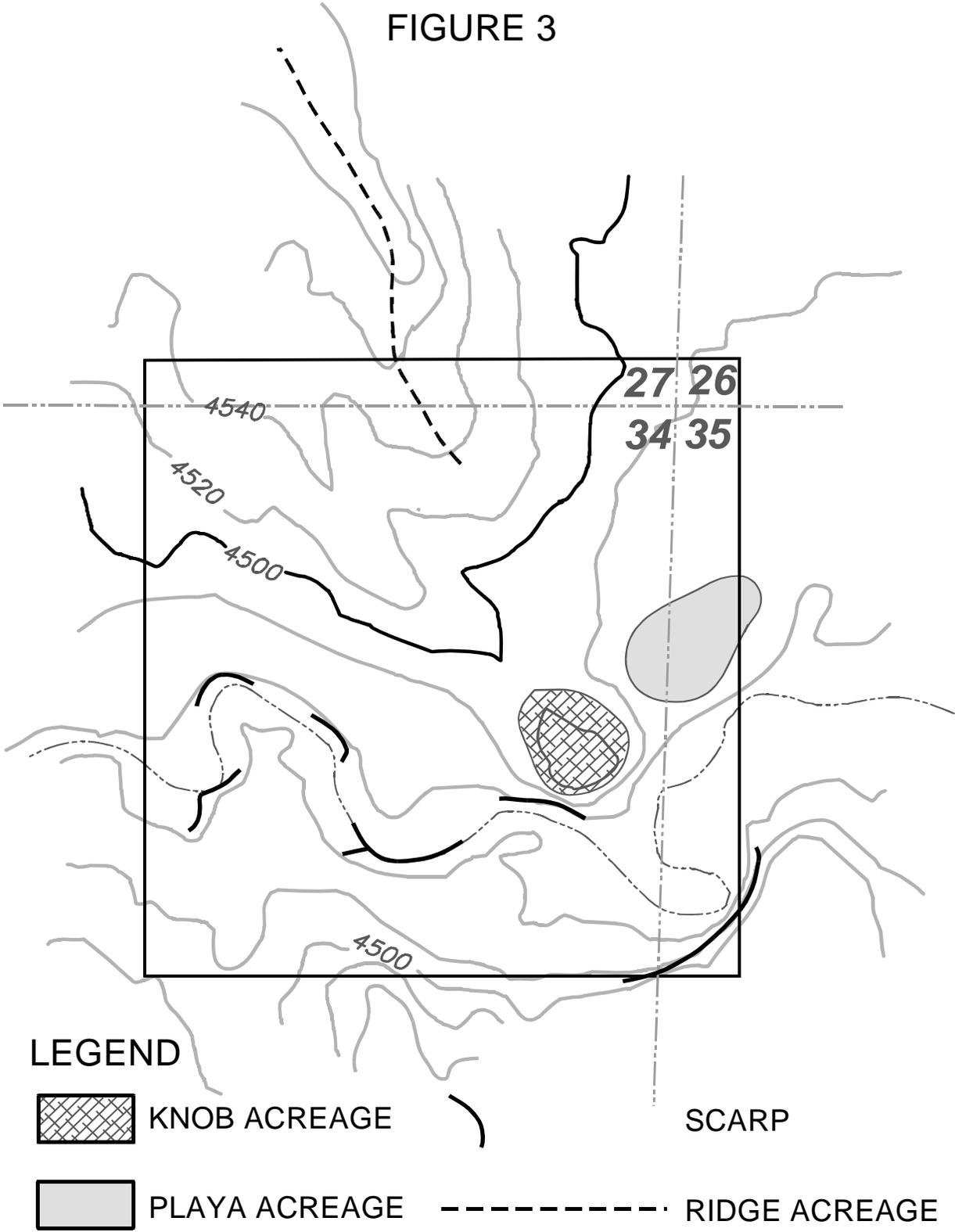


FIGURE 3



## C. References

Perrens, S.J., G.R. Foster, D.B. Beasley. 1984. "Erosion's Effect on Productivity Along Non-Uniform Slopes" In: Erosion and Soil Productivity; Proceedings of the National Symposium on Erosion and Soil Productivity; December 10-11, 1984 (New Orleans, LA). ASAE Publication 8-85. American Society of Agricultural Engineers, St. Joseph, Michigan.

## NOTES